

# High-Order / *hp*-Adaptive Multilevel Methods for Acoustics.

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## 1 Introduction

## 2 Limitation of standard FEMs

## 3 CFEDG

- An overview
- Two-dimensional domain with micro-structures

## 4 Numerics

- Acoustics problems
- Goal-Oriented Error Estimator

## 5 Conclusions

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- Goal:

$$\sum_{\kappa \in T_h} \tilde{\eta}_{\kappa}(u_h) \leq \text{Tol}.$$

- Automatic refinement algorithm:

- ① Start with initial (coarse) grid  $\mathcal{T}_h^{(j=0)}$ .
- ① Compute the numerical solution  $u_h^{(j)}$  on  $\mathcal{T}_h^{(j)}$ .
- ② Compute the local error indicators  $\tilde{\eta}_{\kappa}$ .
- ③ If  $\sum_{\kappa \in \mathcal{T}_h} \tilde{\eta}_{\kappa} \leq \text{Tol} \rightarrow \text{stop}$ . Otherwise, adapt  $S_{h,\vec{p}}$ .
- ④  $j = j + 1$ , and go to step (1).

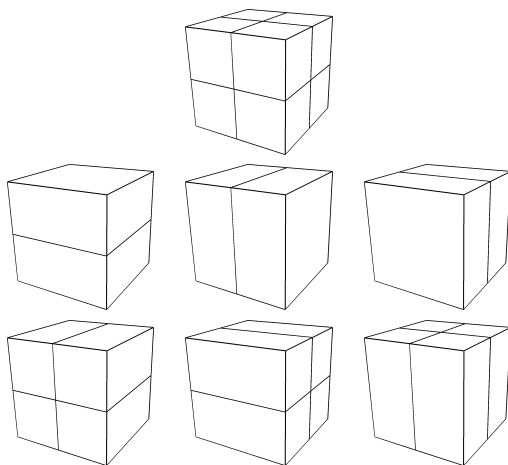
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- **Isotropic  $h$ -refinement:** The marked elements are split in smaller elements
- **Isotropic  $p$ -refinement:** The order of polynomials is increased on the marked elements
- **Isotropic  $hp$ -refinement:** The method automatically chooses to apply either isotropic  $h$ -refinement or isotropic  $p$ -refinement to each marked element



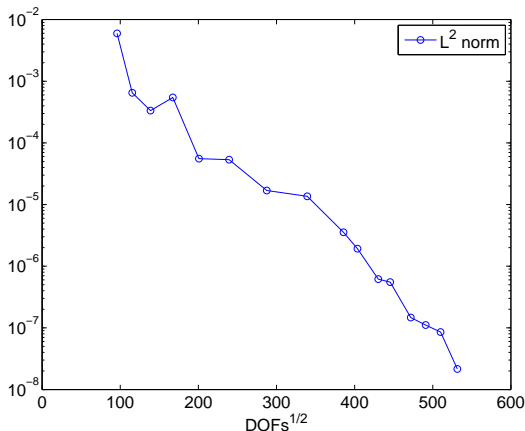
- **Anisotropic  $h$ -refinement:** The method automatically chooses to apply either isotropic or anisotropic  $h$ -refinement to each marked element
- **Anisotropic  $h$ -isotropic  $p$ -refinement:** The method automatically chooses to apply either isotropic/anisotropic  $h$ -refinement or isotropic  $p$ -refinement to each marked element
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$$\Omega \equiv [0, 1]^2, \quad \omega = 30000, \quad c = 331.3 \text{ (air)}, \quad y_0 \equiv (0.51, 0.51)$$

$$-\Delta u - (\omega/c)^2 u = \delta_{y_0} \quad \text{in } \Omega, \quad u = G_{y_0} \quad \text{on } \partial\Omega.$$

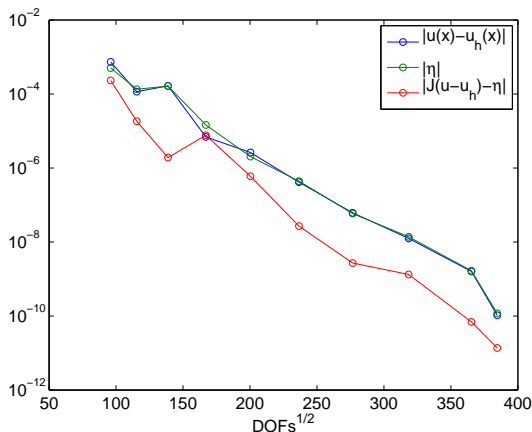
Initial mesh:  $10 \times 10$ ,  $p = 5$



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Initial mesh:  $10 \times 10$ ,  $p = 5$ ,  $J(u) := \int_{\Omega} \delta_{x_0} u$ ,  $x_0 \equiv (0.21, 0.21)$



A. Pietrzyk, "Accuracy of CAE predictions of NVH characteristics of a vehicle body in view of the dispersion in test", Computational modelling and analysis of vehicle body noise and vibration, University of Sussex, March 27-28 2012.

- They testes up to 34 identical (Volvo) vehicles.
- They measured the noise transfer function (NTF) - Acoustic response due to structural excitation.
- The standard deviation was 5dB.



Fahy F. J.

Statistical energy analysis: a wolf in sheep's clothing?

Internoise '93, Leuven, 1993.

Reported a dispersion for beer cans over 10dB.



Kompella M. S., Bernhard B.J.

Measurement of statistical variation of structural-acoustic characteristics of automotive vehicles

SEA Noise and Vibr Conf., 1993.



Kompella M. S., Bernhard B.J.

Variational of structural-acoustic characteristics of automotive vehicles

Noise Control Eng. J., 44 (2) 1996.

Reported a dispersion of 10-20 dB.

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What is limiting standard FEMs in acoustics?

It is the complexity of the geometry.

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Ingredients:

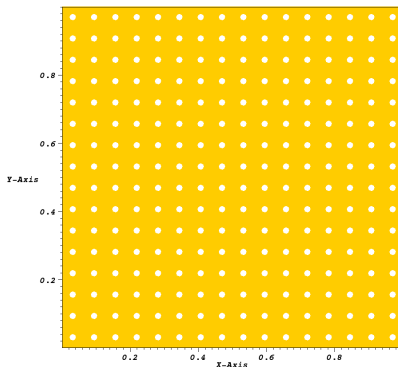
- 1 a mesh  $\mathcal{T}$
- 2 a finite element space  $\mathcal{S}$  constructed on  $\mathcal{T}$

The standard way to construct a finite element space is to associate to each element in the mesh  $\mathcal{T}$  a certain number of DOFs.

More element in the mesh  $\mathcal{T} \Rightarrow$  more DOFs in the finite element space  $\mathcal{S}$ .

More DOFs  $\Rightarrow$  more expensive problem to solve.

## Plate with 256 circular holes



a lot of elements are necessary to describe the geometry and this implies a lot of DOFs.

Thousands of elements  $\Rightarrow$  thousands of DOFs.

DOFs are used to approximate the solution.

So, DOFs should be placed only where it is useful to improve the accuracy of the approximated solution.

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Then for domains with complicated geometries it is common to end up with very big problems to solve and at the same time a very poor accuracy.

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Solution ...

The construction of the finite element space  $S$  should be independent on mesh.



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CFEDG (composite finite element discontinuous Galerkin) method:



P. Antonietti, S.G. and P. Houston

*hp*-version composite discontinuous Galerkin methods for elliptic problems on complicated domains

SISC, submitted.

It is an extension of CFE for continuous Galerkin:



W. Hackbusch and S.A. Sauter

Composite finite elements for the approximation of PDEs on domains with complicated micro-structures

Numer. Math., 75, 447–472, 1997.



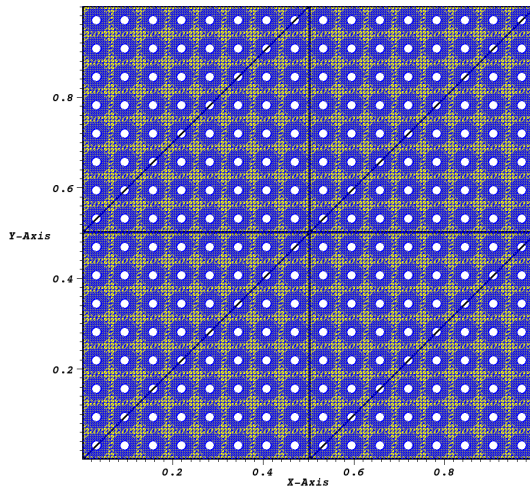
W. Hackbusch and S.A. Sauter

Composite finite elements for problems containing small geometric details. Part II: Implementation and numerical results

Comput. Visual Sci., 1, 15–25, 1997.

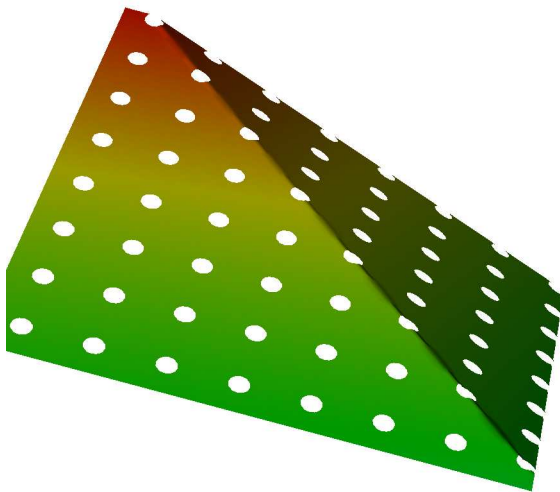
Two meshes:

- Mesh  $\mathcal{T}_{h_\ell}$  is a partition of the domain  $\Omega$  and describes all the details in the domain.
- A coarser mesh  $\mathcal{T}_{\text{CFE}}$  which is too coarse to describe the details in the domain  $\Omega$ .



Transferring information from the fine level to the coarse level:

- 1 The geometrical details are not “stored” in the coarse mesh  $\mathcal{T}_{\text{CFE}}$  but in the finite element basis functions on the coarse level.
- 2 The mesh  $\mathcal{T}_{\text{CFE}}$  and the correspondent finite element space  $V(\mathcal{T}_{\text{CFE}}, p)$  are used to set the size and the sparsity of the linear system.



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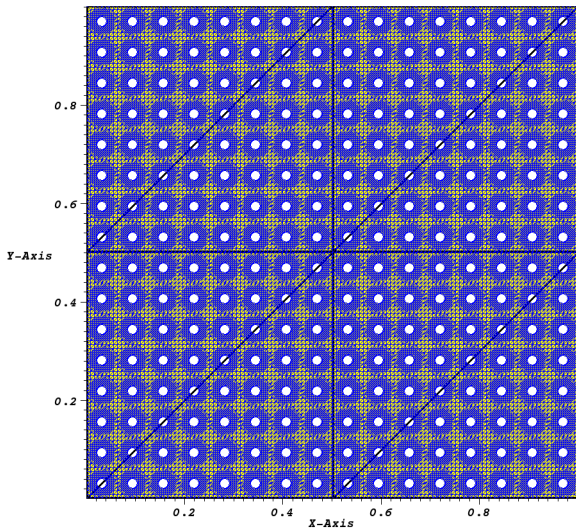
$$-\Delta u = f \text{ in } \Omega,$$

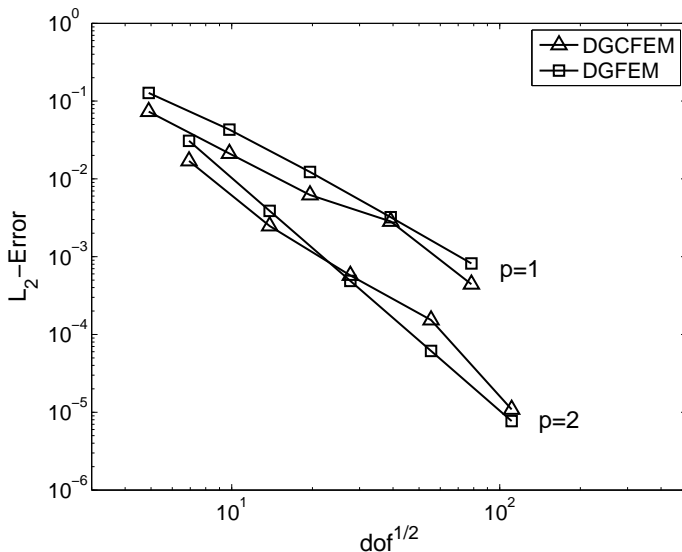
$$u = g \text{ on } \partial\Omega.$$

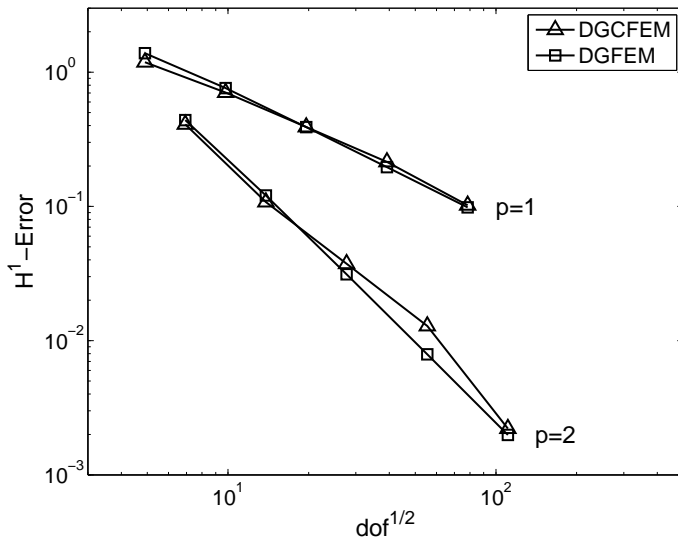
Solution:

$$u = \sin(\pi x) \cos(\pi y).$$

$\Omega$  has micro-structures.







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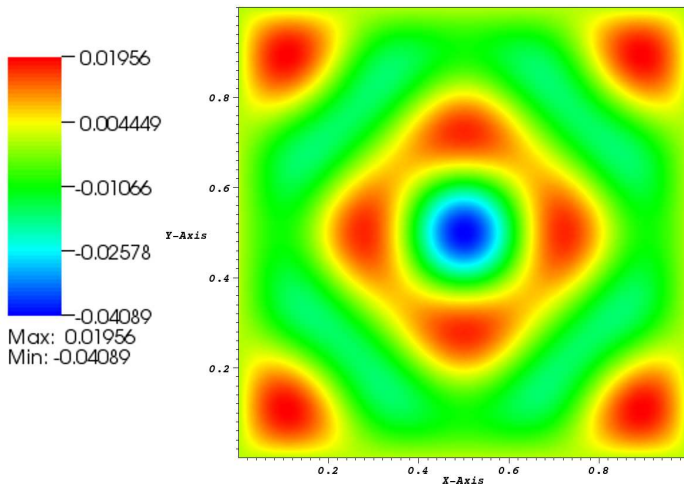
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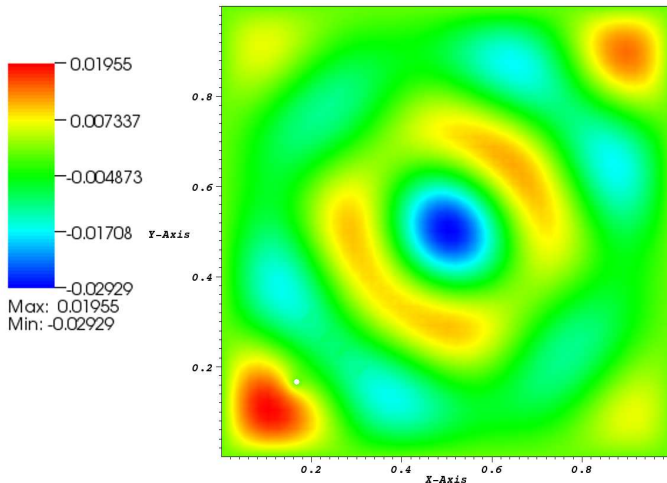
$$-\Delta u - (k/c)^2 u = 1 \text{ in } \Omega,$$

$$u = 0 \text{ on } \partial\Omega.$$

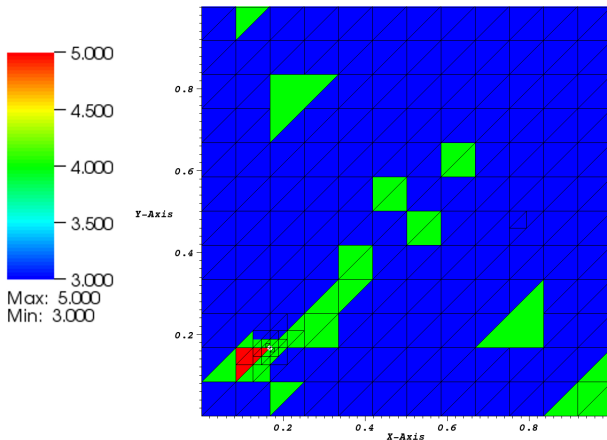
With  $k = 6000$ ,  $c = 331.3$



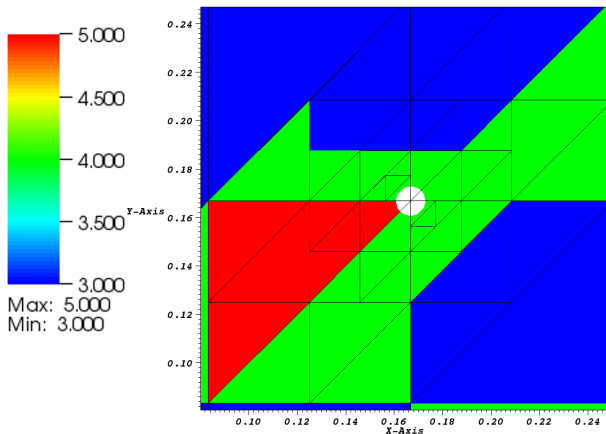




Hole of diameter 0.01.



DOFs: 3597, Elements: 327,  $\|u - u_h\|_0 = 4.5128E-005$



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Primal linear problem:

$$a(u, v) = F(v) .$$

Dual linear problem:

$$a(v, z) = J(v) , \quad J(v) := \int_{\Omega} \delta_{x_0} v .$$

Goal oriented error estimator:  $u_{hp} \in S_{h,\vec{p}}$

$$J(u) - J(u_{hp}) = a(u - u_{hp}, z) = F(z) - a(u_{hp}, z) .$$

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$$J(u) - J(u_{hp}) = a(u - u_{hp}, z) = F(z) - a(u_{hp}, z) = \sum_{\kappa \in \mathcal{T}_h} \tilde{\eta}_{\kappa}(u_{hp}, z) ,$$

$$|J(u) - J(u_{hp})| \leq \sum_{\kappa \in \mathcal{T}_h} |\tilde{\eta}_{\kappa}(u_{hp}, z)| .$$

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Goal oriented error estimator:  $u_{hp} \in S_{h,\vec{p}}$ ,  $\tilde{z}_{hp} \in \tilde{S}_{h,\vec{p}+1}$

$$J(u) - J(u_{hp}) \approx a(u - u_{hp}, \tilde{z}_{hp}) = F(z) - a(u_{hp}, \tilde{z}_{hp}) = \sum_{\kappa \in \mathcal{T}_h} \tilde{\eta}_{\kappa}(u_{hp}, \tilde{z}_{hp}) ,$$

$$|J(u) - J(u_{hp})| \lesssim \sum_{\kappa \in \mathcal{T}_h} |\tilde{\eta}_{\kappa}(u_{hp}, \tilde{z}_{hp})| .$$

Cons:

- ❶ **Expensive:** a dual problem should be solved

Pros:

- ❶ **Flexible:** the quantity of interest can be chosen
- ❷ **Sharp Bound:** the upper bound has constant 1

$$|J(u) - J(u_{hp})| \lesssim \sum_{\kappa \in \mathcal{T}_h} |\tilde{\eta}_{\kappa}(u_{hp}, \tilde{z}_{hp})| .$$

- ❸ **Accurate:** it is possible to compute an accurate estimation of the error in the quantity of interest

$$J(u) - J(u_{hp}) \approx \sum_{\kappa \in \mathcal{T}_h} \tilde{\eta}_{\kappa}(u_{hp}, \tilde{z}_{hp}) ,$$

- ❹ **Improved Accuracy:** it is possible to improve the accuracy of the quantity of interest

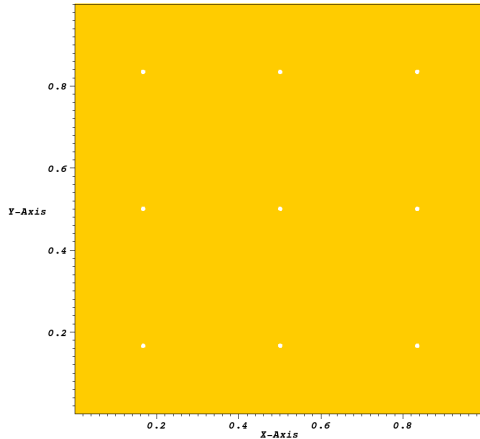
$$J(u) \approx J(u_{hp}) + \sum_{\kappa \in \mathcal{T}_h} \tilde{\eta}_{\kappa}(u_{hp}, \tilde{z}_{hp}) ,$$

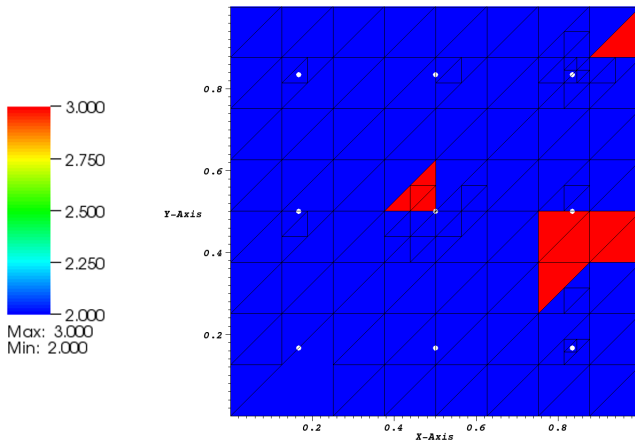


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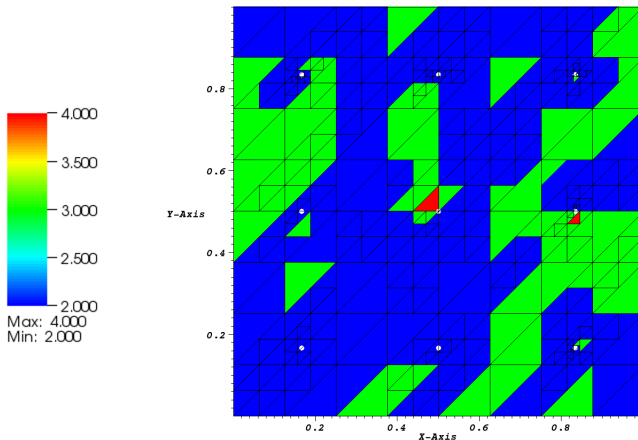
$$u = 0 \text{ on } \partial\Omega.$$

With  $k = 6000$ ,  $c = 331.3$ . The domain has 9 small holes.  
The point of interest is  $(0.71 \ 0.69)$ .





Mesh 6 - DOFs: 1110, Error: -5.4524 dB.



Mesh 9 - DOFs: 3334, Error: -8.6696 dB.

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- ① CFEDG can solve a problem with complicated geometry with few DOFs.
- ② *hp*-adaptivity can introduce new DOFs in an efficient way only where it is important to improve the accuracy of the solution.
- ③ You have full control on the number of DOFs in your system.
- ④ CFEDG can be used as a preconditioner as well.
- ⑤ CFEDG is memory efficient